

1 Programmable Fluidic Networks on Centrifugal Microfluidic Discs

2 Lourdes AN Julius^{a,b}, Sarai M Torres Delgado^c, Rohit Mishra^a, Nigel Kent^{d,e,f}, Eadaoin Carthy^{d,e,f},
3 Jan G Korvink^c, Dario Mager^c, Jens Ducreé^{b,e,f} and David J Kinahan^{d,e,f,g,*}

4 ^a Fraunhofer Project Center at Dublin City University (FPC@DCU), Dublin City University, Glasnevin, Dublin 9, Ireland

5 ^b School of Physical Sciences, Dublin City University, Glasnevin, Dublin 9, Ireland

6 ^c Institute of Microstructure Technology, Karlsruhe Institute of Technology, Hermann-von-Helmholtz-Platz 1, Eggenstein-
7 Lepolshafen 76344, Germany

8 ^d School of Mechanical & Manufacturing Engineering, Dublin City University, Glasnevin, Dublin 9, Ireland

9 ^e National Centre for Sensor Research, Dublin City University, Glasnevin, Dublin 9, Ireland

10 ^f Biodesign Europe, Dublin City University, Glasnevin, Dublin 9, Ireland

11 ^g I-Form, the SFI Research Centre for Advanced Manufacturing, Dublin City University, Dublin 9, Ireland

12 *david.kinahan@dcu.ie

13 ABSTRACT

14 Background:

15 Biomedical diagnostic and lab automation solutions built on the Lab-on-a-Disc (LoaD) platform has great
16 potential due to their independence from specialized micro-pumps and their ease of integration,
17 through direct pipetting, with manual or automated workflows. However, a challenge for all microfluidic
18 chips is their cost of manufacture when each microfluidic disc must be customized for a specific
19 application. In this paper, we present centrifugal discs with programmable fluidic networks.

20 Results:

21 Based on dissolvable film valves, we present two technologies. The first, based on recently introduced
22 pulse-actuated dissolvable film valves, is a centrifugal disc which, depending on how it is loaded, is
23 configured to perform either six sequential reagent releases through one reaction chamber or three
24 sequential reagent releases through two reaction chambers. In the second approach, we use the
25 previously introduced electronic Lab-on-a-Disc (eLoaD) wireless valve array, which can actuate up to 128
26 centrifugo-pneumatic dissolvable film valves in a pre-defined sequence. In this approach we present a
27 disc which can deliver any one of 8 reagent washes to any one of four reaction chambers. We use
28 identical discs to demonstrate the first four sequential washes through two reaction chambers and then
29 two sequential washes through four reaction chambers.

30 Significance:

31 These programmable fluidic networks have the potential to allow a single disc architecture to be applied
32 to multiple different assay types and so can offer a lower-cost and more integrated alternative to the
33 standard combination of micro-titre plate and liquid handling robot. Indeed, it may even be possible to
34 conduct multiple different assays concurrently. This can have the effect of reducing manufacturing costs
35 and streamlining supply-chains and so results in a more accessible diagnostic platform.

36

37 1. Introduction

38 The Lab-on-a-Disc (LoaD) [1–10] offers great potential for point-of-care and point-of-use lab-on-a-chip
39 applications. Some of the key application areas include biomedical diagnostics [1] and environmental

40 monitoring [11]. A significant advantage of the LoAD platform is the ability to perform complex sample
41 preparation steps in an automated fashion, including blood processing [12,13] and solid phase
42 purification of nucleic acids [14–17]. The LoAD platform sits at the interface between low-cost, highly
43 manufacturable and widely used microfluidic diagnostic tests which have little sample preparation
44 requirements, such as lateral flow tests for pregnancy or COVID-19 [18], and specialised and complex
45 diagnostic tests best conducted using liquid handling robotics and specialised instrumentation in
46 centralised facilities.

47

48 A key reason for the LoAD's potential is excellent 'world-to-chip' interfacing [16]. The LoAD does not
49 require specialised micro-pumps to operate, nor does it need to be connected to a pressure source
50 (pump) to operate. It does not require bleeding of trapped air prior to operation or any special liquid
51 loading protocols. In many cases, once loaded with sample and/or reagents (most often through direct
52 manual pipetting), the discs can often be fully sealed from the atmosphere prior to operation and can
53 remain sealed during disposal. This can protect on-disc samples from contamination from the
54 surrounding environment. It can also protect the surrounding environment/laboratory from
55 contamination by samples, particularly critical for highly sensitive nucleic acid amplification-based
56 assays (e.g., PCR, LAMP, RPA). Ease of sample loading also permits integration of automated robotics
57 system with centrifugal microfluidic [19].

58

59 The increasing availability of low-cost micro-controllers and electronics, primarily driven by the
60 smartphone, has made combining the Lab-on-a-Disc with co-rotating electronics feasible. While these
61 platforms, broadly called Electronic Lab-on-a-Disc (eLoAD) [20], can use electrical slip rings [21], they
62 typically use wireless power transfer and wireless communication protocols such as Bluetooth or WiFi. A
63 key advantage of this approach is it enables easier measurement from the disc, as sensors can co-rotate
64 with the microfluidic disc. Applications of providing power and communication to the disc have included
65 electrochemical measurements [21–23], chemiluminescence [24], colorimetric measurements [25],
66 centripetal pumping [26,27], nucleic acid amplification [28,29], and flow control [12,30].

67

68 As centrifugation applies pressure to all liquids on the LoAD, reliable valving technology is critical to
69 automating laboratory assays. Passive valves such as capillary valves [31] are opened by stepped
70 increases in disc spin-rate, while siphon valves [32] are opened by decreases in disc spin-rate. Due to
71 limitations of passive valves, mainly driven by a limit in the number of valves which can be accurately
72 controlled in a defined sequence (and so placing a limit on the number of laboratory operations which
73 can be automated), active valves, which use additional instrumentation to interact with the disc to open
74 or close a valve, have been of increased recent interest [33]. The integration of dissolvable films (DF)
75 into the LoAD [34], and particularly the development of DF-enabled pneumatic networks called event-
76 triggered valves [17], has allowed increased complexity of on-disc liquid flow control using motor-only
77 control. Conventional DF valves have been applied to colorimetric measurements [35] and cancer
78 diagnostics [36,37] while even-triggered valves have been applied to epilepsy [38], immunoassays [39–
79 41], white blood cell isolation [42], serial dilutions [43] and solid phase purification of nucleic acids
80 [16,17,44]. Furthermore, liquid-specific dissolvable films (i.e. dissolving in oil rather than water) have
81 also been used to automate assays [45]. In an active valving approach, DF valves have also been

82 integrated with the eLoaD concept [12], allowing up to 64 valves be wirelessly opened on demand.
83 Recently, Mishra et al. [46] introduced a new type of DF valve called 'digital pulse actuated' (PA-DF)
84 valves. Here, the event-triggered network is combined with DFs in recessed gas pockets such that the
85 architecture of the disc defines the sequence valves open while short, pulsed increases in disc spin-rate
86 control the timing of valve actuation.

87
88 Programmable fluid networks have been presented by the microfluidics community in several different
89 forms. Lutz et al. [47] demonstrated the use of programmable elements in paper microfluidics to vary
90 the timing of an assay. Zhakypov [48] create programmable fluidic networks by using a robot to fold an
91 origami structure into different configurations. Tsuda et al. [49] demonstrated a plug-and-play approach
92 using 3D printed components while Zucchelli et al. [50] have described on-demand creation of networks
93 of connecting microchannels using laser ablation in centrifugal microfluidics.

94
95 This work presents two approaches to creating a programmable fluidic network on a LoaD. These
96 programmable networks, which leveraging pre-existing valve platforms, represent the key novelty of
97 this work. We demonstrate how the behaviour of a disc can be programmed using control software
98 (software defined network using the eLoaD) and then how a disc can be programmed using the
99 sequence and loading of reagents on-disc (reagent defined network).

100
101 While Zucchelli et al. [50] implement programmable networks on the LoaD, their system, based on laser
102 ablation, would not be suitable for applications at point-of-care or point-of-use. The eLoaD
103 implementation presented here is designed as a low-cost instrument solution for use in resource limited
104 settings while the reagent-defined system needs just a low-cost spindle motor to operate.

105
106
107 Firstly, we build on the previously introduced LoaD-controlled Parafilm™ valve platform [12] to present
108 a system which can be defined using software control (wirelessly over Bluetooth™ or similar). This
109 expands the capability of the eLoaD valving technology and, as far as we are aware, introduces an
110 entirely novel approach to defining disc architectures. In our second approach, we combine our recently
111 introduced pulse-actuated DF valves [46] in a novel fashion with AND and OR conditional actuation to
112 define disc architectures based on order in which reagents are loaded on-disc.

113
114 For the eLoaD-controlled platform, the disc is aligned with an array of co-rotating microheaters. These
115 microheaters can melt a Parafilm™ (wax) seal, which triggers the release of liquid through a dissolvable
116 film. In this disc, we have 8 reagent chambers (numbered 1-8) and four reaction chambers (labelled A-
117 D). Between each reagent chamber is four valves and, by opening one of these valves, the liquid can be
118 routed to the appropriate reaction chamber. Thus, by opening the valves in a defined sequence, any
119 combination of reagents can be routed to any combination of valves. To demonstrate this functionality,
120 we first configure the disc such that Reagents 1-4 are routed to Chamber A and Reagents 5-8 are routed
121 to Chamber B. Then, using an identical disc, we configure the system such that Reagents 1-2 are routed to
122 Chamber C, Reagents 3-4 to Chamber B, Reagents 5-6 to Chamber A, and Reagents 7-8 to Chamber D
123 (Figure 1 and Figure 2).

124
125 Our architecture based on pulse-actuated DF valves [46] leverages the ability of these DF-based valves to
126 implement AND and OR conditional actuation. This provides a system which is controlled by reagents
127 loaded on disc. The disc has seven reagent chambers. Loading chambers 1-6 results in a sequential
128 release, with each pulse in spin-rate, of reagents in chambers 1-6. However, loading chambers 1-3 and
129 5-7, on an identical disc, results in parallel release of reagent from chambers 1 and 7 on the first pulse,
130 chambers 2 and 6 on the second pulse, and chambers 3 and 5 on the third pulse (Figure 3 and Figure 4).
131 Thus, it is possible to complete two different sets of liquid handling operations using the same disc
132 architecture.

133
134 In this paper, we describe the design and architecture of these programmable fluidic networks and, as a
135 first step, demonstrate their functionality using dyed water. We then discuss their potential, with
136 further advancement, to provide a flexible complementary technology to the microplate where the
137 ability to program a microfluidic chip to be compatible with a wide range of assays can allow the discs to
138 be mass manufactured at a low-cost. The architectures presented here represent a first step towards
139 flexible fluidic networks which, with further refinement, may be suitable for applications across a wide
140 range of different bio-assays.

141

142 **2. Materials and Methods**

143 **2.1 Disc Manufacture and Assembly**

144 The microfluidic discs used in this study were assembled from either eight or twelve layers of material,
145 depending on if they used PA-DF or eLoaD actuated DF valves, respectively. As previously described by
146 Kinahan et al. [17], for PA-DF valves, these layers were four layers of 0.086 mm pressure sensitive
147 adhesive (PSA) (Adhesives Research, Limerick, Ireland) and four layers of poly(methyl methacrylate)
148 (PMMA). The PMMA layers were laser cut (Epilog Zing, USA) to generate air-vents, reservoirs for liquids,
149 and connecting holes vertically through the disc while microchannels were created in the PSA using a
150 knife cutter (Graphtec, Yokohama, Japan). Briefly and listed from the top, Layer 1 (0.5 mm PMMA)
151 contains loading and air vents. Layer 2 (PSA) contains upper-level microchannels for liquid movement
152 and pneumatic venting, Layer 3 (1.5 mm PMMA) primarily defined large reservoirs for liquid, Layer 4
153 (PSA) and Layer 5 (PSA) were layers to sandwich and support DF tabs, Layer 6 (0.5 mm PMMA)
154 contained through-holes and Layer 7 (PSA) contained microchannels for liquid movement and
155 pneumatic venting. Finally, Layer 8 (PMMA 0.5mm) was the sealing layer on the underside of the disc.

156

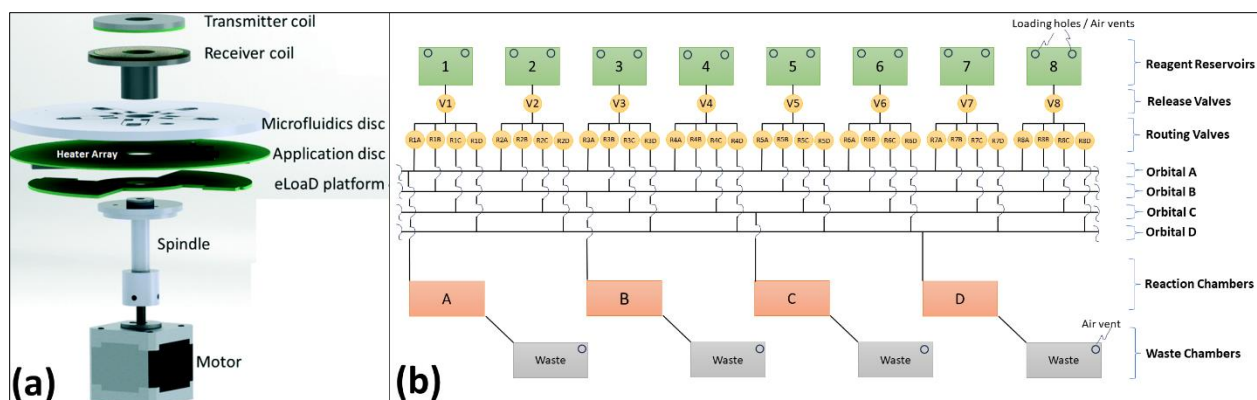


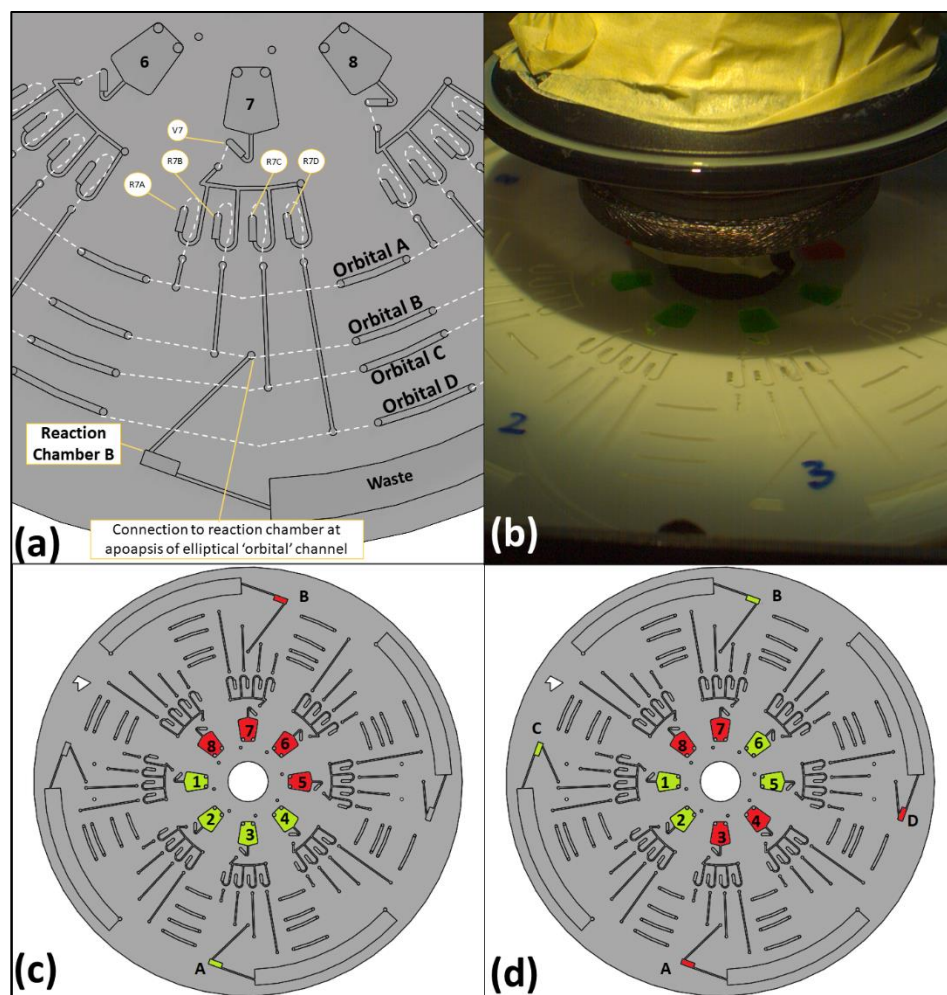
Figure 1: Configuration of the wireless eLoaD platform (Reproduced from Ref. [24] with permission from the Royal Society of Chemistry) (b) schematic of the fluidic network enabled by the eLoaD platform

For the eLoaD actuated DF valves, a similar architecture was used, which was adapted from that presented by Delgado et al. [12]. The first seven layers of this disc have a similar configuration to that described above; however, for the eLoaD actuated valves, Layer 8 (0.5 mm PMMA) contains through-holes which can act as pneumatic venting holes. Layer 9 (PSA) and Layer 11 (PSA), and Layer 12 (0.5 mm PMMA) mirrored the heater elements on the eLoaD application disc while Layer 10 (Parafilm™) is a single layer of wax Parafilm™ which seals the valves on the disc.

2.2 Test Stand and eLoaD

The discs used in this study were imaged using a test-stand which is previously described [12]. Briefly, a spindle motor (Festo EMME-AS-55-M-LS-TS, Esslingen, Germany) is synchronised with a sensitive, short-exposure time camera (Basler Ace 2040-90uc, Basler, Germany) and a stroboscopic light source (Drelloscop 3244, Drello, Germany) using a trigger output signal from the motor. A series of still images are acquired at 5 Hz and, due to synchronisation, it can appear the disc is stationary. These images are later used to create videos provided in ESI. This system is controlled using a custom LabVIEW program.

The eLoaD [12,20,24,25,27] comprises an Arduino compatible microcontroller and a wireless power receiver. The receiver is part of the 5W-series of Qi Standard for wireless power transfer. Power transmission is from a standard wireless phone charger amounted above the disc as previously described [12,24]. The 'application disc', fitted to the eLoaD, is a 120 mm diameter PCB board with 128 micro-heaters, and, as previously described, each of these heaters can be individually activated remotely using Bluetooth control via custom software [12].



182
 183
 184 Figure 2: The operation of the programmable fluidic networks using the eLoaD system. (a) shows a detail of one of the
 185 reservoirs on the Lab-on-a-Disc. Each reservoir is closed with a DF valve which can be activated by a heater on the eLoaD. After
 186 this valve, the fluid is connected via four valves to four 'orbital' channels, which extend around the entire disc. These orbitals
 187 are connected at their periapsis to a reaction chamber (b) shows the disc mounted on the eLoaD system with power
 188 transmission from above via a commercial phone charger (c-d) show schematics of the entire discs (c) is configured to wash two
 189 reaction chambers with four reagents (d) is configured to wash four reaction chambers with two reagents each (see ESI Movie
 190 1, 1a, 2 and 2a)

191 When testing the Pulse-Actuated programmable networks, the discs are fitted directly to the spindle
 192 motor, and the camera is in a top-down orientation. However, for testing with the ferro-wax controlled
 193 valves, the discs are aligned with the eLoaD application disc using alignment pins and then placed on
 194 the spindle motor. The transmitter is then placed above the discs. Due to the positioning of the
 195 transmitter, the camera and the strobe are oriented at an angle to image as much of the disc as
 196 possible.

197 198 3. Operation of Programmable Networks

199 *Programmable Fluidic Network using eLoaD*

200 The programmable fluidic network using the eLoaD consists of 8 reservoirs located at the centre of the
 201 disc, which can be connected in any combination to four reaction chambers located radially outwards
 202 (Figure 1 and Figure 2). Each reservoir is sealed by a corresponding valve (i.e. V1 through V8) which can

203 be actuated by the eLoaD system and is used for reagent release (reagent valve). Past this valve, the
 204 channel splits into four and each of these channels is sealed by valves which are used for routing
 205 (routing valve) (in the case of Reservoir 1, referred to as R1A, R1B, R1C and R1D). Each of these valves
 206 is, in turn, connected to an elliptical channel, which is connected all around the disc, which we refer to
 207 as an orbital channel. R1A, along with R2A through R8A, are all connected to Orbital A. Orbitals B-D are
 208 all connected in a similar manner. At the radially outwards location of these orbitals (i.e. the periapsis),
 209 there is a reaction to the corresponding reaction chamber and waste chamber. The connection at the
 210 periapsis ensures that the reservoirs empty through the reaction chamber in an efficient manner.
 211

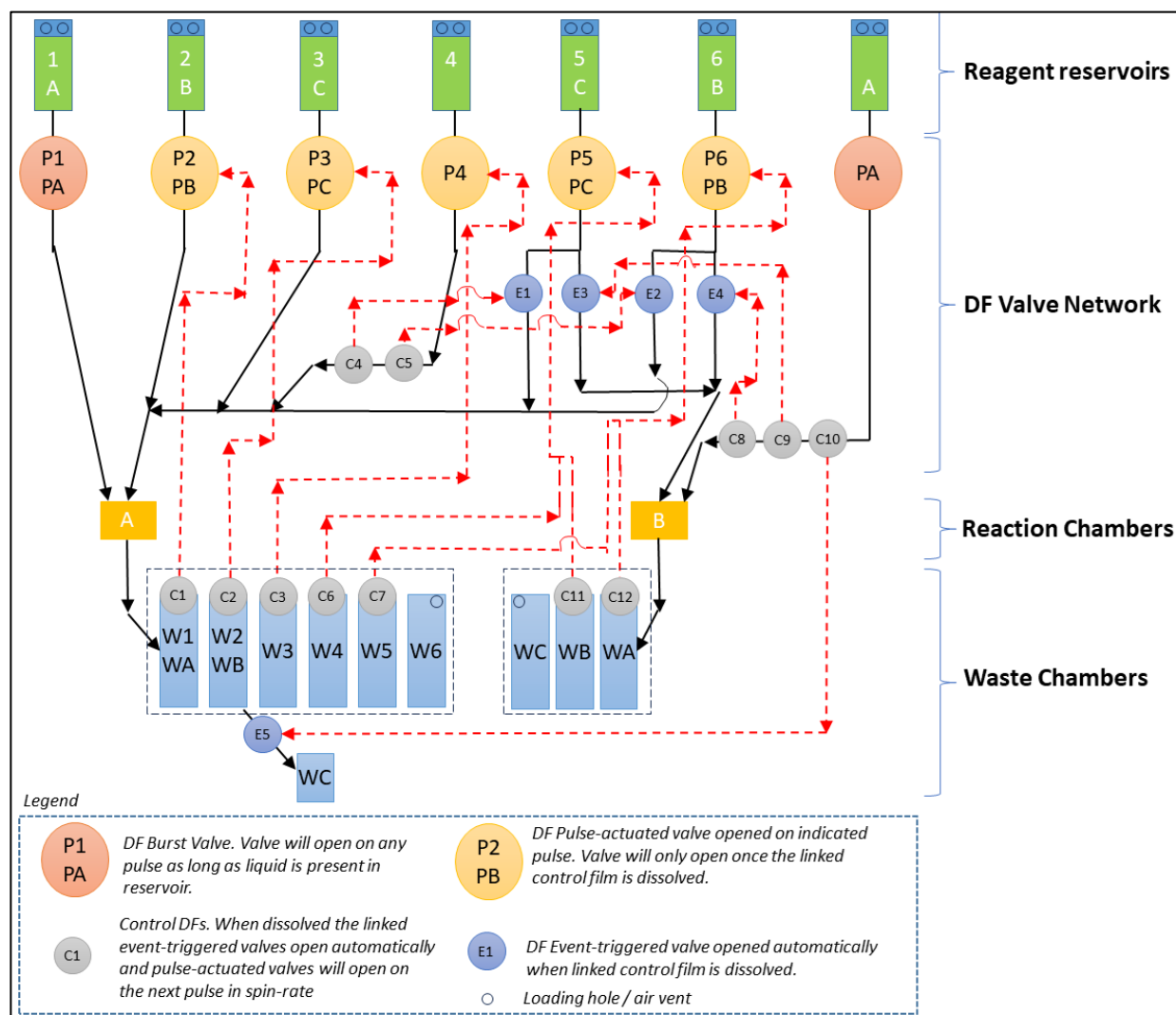
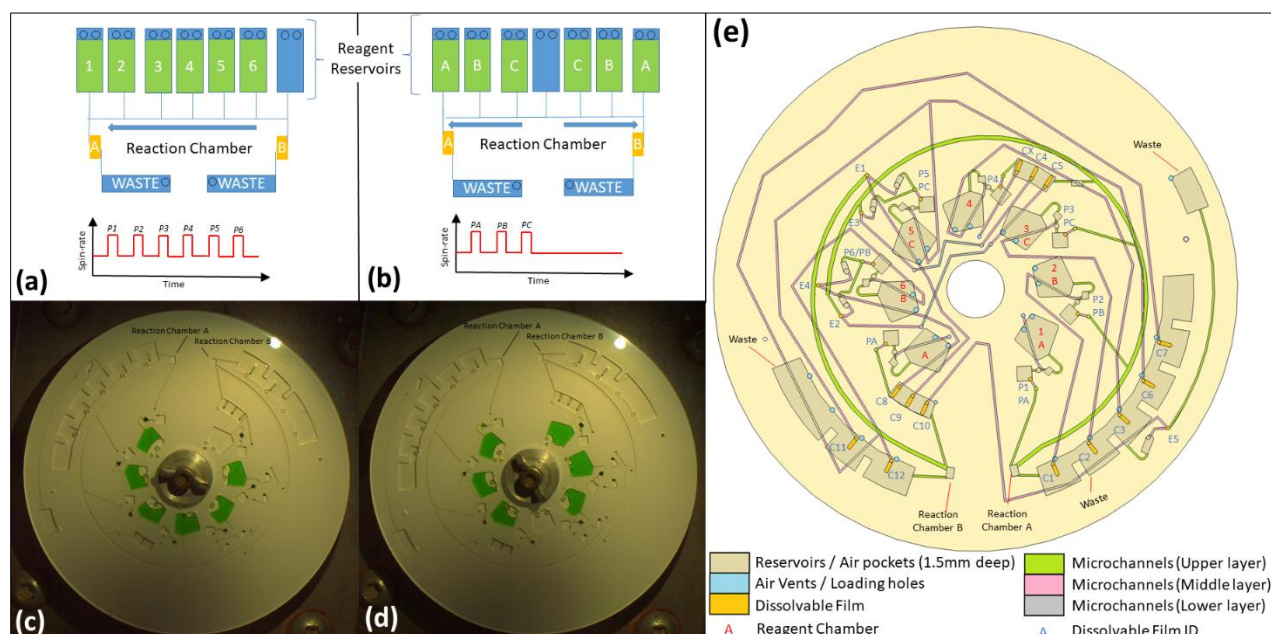


Figure 3: Schematic of the fluidic network which enabling the rotational controlled disc

212
 213
 214
 215 To operate the disc in the configuration shown in Figure 2c (see also ESI Movie 1), the disc is mounted
 216 on the eLoaD system, and the chambers are loaded. Next, the Parafilm™ wax sealing valves R1A, R2A,
 217 R3A and R4A are melted using the corresponding heaters on the eLoaD. R5B, R6B, R7B and R8B are also
 218 opened. With this configuration in place, opening V1 will release the liquid in Reservoir 1 to flow into
 219 and through valve R1A and on into Reaction Chamber A. Reservoirs 2-4 can, in turn, be opened on-
 220 demand (i.e. programmatically or using a UI) and will all be routed to Chamber A. Reservoirs 5-7 can also
 221 be opened on-demand and routed through Reaction Chamber B.

222
223
224
225
226
227
228
229
230
231
232

For the configuration shown in Figure 2d (see also ESI Movie 2), where four reaction chambers are washed with two reagents each, the routing valves R1B, R2B, R3A, R4A, R5C, R6C, R7D and R8D are used to program the fluidic network. From here, as each valve is actuated, the liquid is directed through the correct routing chamber. Note that in ESI Movie 2, Valve 2 fails to open due to a manufacturing defect associated with the manual assembly of these discs. It should also be noted that this same liquid handling sequence can be managed by just the routing valves if the reagent valves were removed or pre-opened. However, we have conceptually divided the design into valves which define fluidic routing / disc architecture (routing valves) and those which define the assay release.



233
234
235
236
237
238
239
240
241
242
243
244
245
246
247
248
249
250
251
252

Figure 4: The operation of the programmable fluidic network using pulse actuated dissolvable film valves. Here, the way the disc is loaded determines the sequence of reagent release. These are (a) six reagents through one reservoir and (b) three reagents through two reservoirs. In (a), chambers 1-6 are loaded and six digital pulses are used to wash the content of the six reservoirs through reaction chamber A, while (b) shows a configuration where chambers 1-3 and 5-7 are loaded. Here, three pulses will wash the contents of chambers 1-3 through reaction chamber A and the contents of chambers 7-5 (in that order) through reaction chamber B. Note in the 6x1 configuration, the pulses are P1-P6 while in the 3x2 configuration, we refer to the three pulses as PA, PB and PC respectively. (c) and (d) show the discs loaded to operate in the 6x1 and 3x2 configurations, respectively (see also ESI Movie 3, 3a, 4 and 4a) (e) shows detail colour coded schematic of the fluidic network including intermediate and lower connecting channels not shown in other figures.

Programmable Fluidic Network using Pulse Actuated Valves

As described previously, DF-based event-triggered valves can be configured to enable AND and OR operations on-disc [17]. In an alternative approach to using the eLoaD, we have combined this principle with pulse actuated DF valves [46] to develop a disc which can be programmed based on how the reagents are loaded. Namely, as shown in Figures 3 and 4, an identical disc can be loaded to release reagents in a 6x1 configuration (six reagents through one reaction chamber) or 3x2, where three reagents are each released through two reaction chambers. In this description, we adapt the terminology used previously [46] to describe the pulse actuated valves and use four key terms which are highlighted in the legend shown in Figure 3.

- 253 • DF Burst valves are opened when the disc exceeds a design opening spin frequency. Here, the
254 DF is recessed in an air pocket as previously described [34,36].
- 255 • DF Pulse-actuatedValves valves [46] are composed of two DFs. The Load film (LF) is the DF
256 through which the liquid is released, while the control film (CF) vents part of the valve. For pulse
257 actuated valves, when the CF is sealed, the vales will not open at any spin frequency within the
258 design envelope of the disc (in our case, it will not open at any speed below 100 Hz). With the
259 CF dissolved, the valve partially vents and so can be opened, in a manner like a burst valve, by
260 exceeding a design spin-rate (in our case, 40 Hz). We refer to this as putting the valve in a
261 'ready' state. Opening the valves with a digital pulse (an acceleration to 50 Hz and then
262 deceleration to 30 Hz) in a time shorter than it takes for the DFs to dissolve allows each valve to
263 be opened in the designed order. The architecture of the disc determines the order the valves
264 open, while the digital pulses in spin-rate determine the timing of valve actuation. In this work,
265 we use OR relationships whereby a valve may have one Load Film (LF) and two or more control
266 films (CFs). Dissolving just one of these CFs will put the valve in a ready state to open on the
267 next pulse. In the following description, we refer to the Load Films (LFs) by the pulse in which
268 they will open (e.g. P1, P2 etc).
- 269 • DF Event-triggered valves [17] are also composed of two DFs referred to as the Load Film (LF)
270 and Control Film (CF). Here, the dissolving of the CF results in the automatic release of liquid
271 through the LF.
- 272 • Control DFs (CFs) are the control films referred to which are part of DF Pulse-actuated valves
273 and DF Event-triggered valves. Dissolving these films, by reagent washing over them or by
274 reagent filling a waste chamber, is key to the operation of the pneumatic network.

275
276 The programmable network of the disc is described in Figure 3, where the path of liquid is shown in
277 black solid lines while pneumatic venting channels are shown in red dashed lines. Consider first that
278 reservoirs 1-6 are loaded and then released by pulses 1-6. The following sequence takes place:

- 280 • On Pulse 1 (P1), the liquid in Reservoir 1 is released and washes through Reaction Chamber A. It
281 flows into waste chamber W1, filling it and dissolving control film C1. With C1 dissolved, valve
282 P2 can open on the next pulse
- 283 • On Pulse 2 (P2), the liquid in Reservoir 2 is released and washes through Reaction Chamber A. It
284 flows into waste chamber W1, and because this chamber is full, the liquid overflows and fills
285 waste chamber W2 (i.e. AND criteria), where control film C2 is wetted and dissolves. With C2
286 dissolved, valve P3 can open on the next pulse.
- 287 • On Pulse 3 (P3), the liquid in Reservoir 3 is released and washes through Reaction Chamber A.
288 Combined with the liquid released from Reservoir 1 and Reservoir 2, waste chambers 1, 2 and 3
289 now fill, and control film C3 is wetted and dissolves. With C3 dissolved, valve P4 can open on the
290 next pulse.
- 291 • On Pulse 4 (P4), the liquid in Reservoir 4 is released. Before washing through reaction chamber
292 A, it washes over control films C4 and C5. These open event-triggered valves E1 and E2. With
293 these valves open, the contents of Reservoir 5 and Reservoir 6 will be routed to Reaction
294 Chamber A on subsequent pulses in disc spin-rate. The liquid in Reservoir 4 continues through
295 Reaction Chamber A and fills the waste chambers such that control film C6 is wetted and
296 dissolves. With C6 dissolved, P5 can open on the next pulse. Note that P5 is controlled by an OR

297 relationship whereby dissolving C6 OR C11 will put P5 in a ready state. Note also that CX (not
298 shown in Figure 3 but shown in Figure 4) is also dissolved. This opens this chamber to
299 atmosphere. It is otherwise sealed to prevent reagents released on P1 or P2 backflowing to
300 incorrectly wet C4 or C5.

- 301 • On Pulse 5 (P5), the liquid in Reservoir 5 is released and is selectively routed (through E1, which
302 was opened in the previous step) to wash through Reaction Chamber A. C7 is now wetted to put
303 P6 in a ready state.
- 304 • On Pulse 6 (P6), Reservoir 6 is released and is selectively routed (through E2, which was opened
305 in the previous step) to wash through Reaction Chamber A and so completing the protocol.

306
307 In the alternative protocol, where Chamber 1-3 and Chambers 5-7 are loaded, the pulses are referred to
308 as Pulse A, Pulse B and Pulse C:

- 309
310 • On Pulse A (PA), the liquid is simultaneously released from Reservoir 1 and Reservoir 7 and
311 washes through Reaction Chamber A and Reaction Chamber B, respectively. As the liquid in
312 Reservoir 7 flows to Chamber B, it wets and dissolves control films C8, C9 and C10. C8 and C9
313 open valves E3 and E4, respectively, which will route the liquid in Chamber 6 and Chamber 5 to
314 be routed through Reaction Chamber B. Dissolving C10 opens valve E5. This acts as a failsafe by
315 opening an overflow chamber. This overflow chamber prevents liquid, which is washed through
316 Reaction Chamber A, from wetting control valves C6 or C7 (which would put valves in a ready
317 state in the wrong order). Control films C1 and C12 are wetted, which puts the valves on
318 Reservoir 2 and Reservoir 6 into a ready state.
- 319 • On Pulse B (PB), the liquid is released from Reservoir 2 and Reservoir 6 and these wash through
320 Reaction Chamber A and Reaction Chamber B, respectively. Control films C2 and C11 are
321 wetted, which puts the valves on Reservoir 3 and Reservoir 5 into a ready state.
- 322 • On Pulse C (PC), the liquid is released from Reservoir 3 and Reservoir 5 and these wash through
323 Reaction Chamber A and Reaction Chamber B, respectively, and so completing the protocol.

324
325 The operation of the discs in these programmed states is shown in ESI Movie 3 and ESI Movie 4,
326 respectively.

327 328 **4. Conclusions and Outlook**

329 One of the major challenges in the widespread adoption of point-of-care diagnostics tests is the cost of
330 manufacture. High-volume manufacture requires roll-to-roll, injection moulding, and automation (i.e.
331 pick and place etc.), which requires significant upfront capital investment. Minor changes to an assay
332 can require development of an entirely new tooling. In addition, these tooling changes can take
333 significant lead-time and optimisation and so may not be quickly available to address emerging
334 challenges such as the next global pandemic. While disc manufacture by injection moulding has been
335 demonstrated [51], discs with embedded DFs have not yet been mass-manufactured. However, it is
336 clear that mass manufacture using injection moulding is possible by integrating automated pick-and-
337 place of DF tabs into the production process. Similarly, it is possible to manufacture DF enabled discs
338 using roll-to-roll by multi-lamination manufacture whereby a whole sheet (of relatively low-cost) DF
339 becomes a layer in the disc supported (and in parts shielded from reagents) by PSA.

340
341 Integration of wax membranes into injection moulded discs using pick-and-place, or a full disc sized
342 sheet of wax Parafilm™ in discs made using roll-to-roll, may also applications towards challenges in wet

343 reagent storage [45].

344

345 Here, we present preliminary work on developing a programmable Lab-on-a-Disc which can be
346 reconfigured to address different liquid handling challenges. We demonstrate this using the low-cost
347 eLaoD platform and using pulse-actuated valves, which only require a spindle motor to function. In this
348 paper, we refer to 'reaction chambers' through which the liquid is washed. The next key step to
349 developing this technology further will be the development of modular reaction chambers. Because the
350 Lab-on-a-Disc does not need to be primed before use, an insert might easily be placed into the Lab-on-a-
351 Disc. This insert might be a silica substrate to enable Solid phase DNA / RNA purification, or it might be
352 an antibody-coated surface to enable an ELISA. The use of such modular inserts, combined with loading
353 the appropriate reagents (which might also occur using modular inserts), would allow the same
354 programmable architecture to be used across a wide range of assays (such as the aforementioned
355 nucleic acid tests or ELISA tests), and so reducing the cost of manufacture. These different assays might
356 be conducted in series (using outputs from one test to inform the second test), or concurrently on the
357 same disc if enough chambers are available. It must be noted that this manuscript demonstrates
358 programmable fluidic networks only the perspective of liquid handling (using dyed water). For next
359 steps, we hope to demonstrate the capability of these platforms to automate two different assays
360 through use of modular reaction chambers discussed above.

361

362 A challenge to commercial deployment of this platform is the reliability of (the relatively complex)
363 microfluidic discs. In this work, the reliability of discs (which were manufacture using manual processes)
364 was ~90% for reagent defined discs and ~70% for the discs which couple to the eLoaD. The difference is
365 primarily due to the additional layers using parafilm for these valves. Automated manufacture would
366 greatly improve reliability of this manufacturing. However, event minor design changes might have
367 knock-on effects to disc reliability which in turn may take significant time to identify and engineer out of
368 the system. Thus, the ability to provide a completely standard disc which can be programmed for
369 multiple applications provides scope to greatly increase reliability. Indeed, there may even be potential
370 to include error-correction architectures which compensate for manufacturing errors as they occur.

371

372

373

374 This technology has great potential in both point-of-care applications and in potential use in laboratory
375 automation. In the first case, these flexible discs might be manufactured as a strategic reserve whereby,
376 in the event of a global health emergency, they can be rapidly loaded with a modular reaction chamber,
377 appropriate reagents, and deployed without the need to start from zero. In the event of a major global
378 emergency, these will act as a stop-gap diagnostic test while cheaper and more specialised options are
379 developed; in the event of a smaller-scale outbreak, their rapid availability might be key to preventing the
380 development of a pandemic. In the case of laboratory automation, with further development, these
381 discs might be integrated into liquid handling units and used as an alternative to micro-titre plates in
382 centralised laboratories. A single-chip architecture which can be applied across a range of tests would
383 greatly minimise cost and logistics while the inherent ability to centrifuge samples on-chip would be
384 particularly useful for hospital labs working on blood samples. While the concept of flexible

385 programmable networks has great potential, it is also clear that application of a single architecture to a
386 range of different assays will have significant challenges. These include potential regulatory issues along
387 with challenges surrounding reagent storage and metering, surface treatments to suit specific assays,
388 and the challenge of integrating different measurement techniques into a standardised platform. We
389 hope that further research will address some of these challenges.

390
391 Furthermore, while a standardised flexible programmable network might address several different
392 assays, no one network will be able to address the entire range of available biomedical diagnostic tests.
393 Indeed, there will also be some assays, such as those requiring long incubations, which cannot be easily
394 addressed by discs which are based on single-use normally closed valves such as the DFs which underpin
395 this paper. From this perspective, there integration of other valve types into the flexible fluidic network,
396 particularly (repeatably) openable / closable valves, leaves significant space for future innovation.

397
398 **Declaration of Competing Interest**
399 The authors declare that they have no known competing financial interests or personal relationships
400 that could have appeared to influence the work reported in this paper.

401
402 **Acknowledgements**
403 This work was partly funded by the European Union under Grant number FP7-KBBE-2013-7-613908-
404 DECATHLON and Grant number H2020-FETOPEN-1-2016-2017-737043-TISuMR, by the Science
405 Foundation Ireland (SFI) and Fraunhofer-Gesellschaft under the SFI Strategic Partnership Programme
406 Grant Number 16/SPP/3321, by the National Council of Science and Technology, CONACyT (Mexico), by
407 the University of Freiburg (Germany), and by Karlsruhe Institute of Technology (Germany). This
408 publication has emanated from research supported in part by a grant from Science Foundation Ireland
409 under Grant numbers 10/CE/B1821 and 16/RC/3872. For the purpose of Open Access, the author has
410 applied a CC BY public copyright licence to any Author Accepted Manuscript version arising from this
411 submission.

412

- 413 **REFERENCES**
- 414 [1] R. Gorkin, J. Park, J. Siegrist, M. Amasia, B.S. Lee, J.-M. Park, J. Kim, H. Kim, M. Ma-
415 dou, Y.-K. Cho, Centrifugal microfluidics for biomedical applications, *Lab on a Chip*. 10
416 (2010) 1758–1773.
 - 417 [2] O. Strohmeier, M. Keller, F. Schwemmer, S. Zehnle, D. Mark, F. von Stetten, R. Zengerle,
418 N. Paust, Centrifugal microfluidic platforms: advanced unit operations and applications,
419 *Chemical Society Reviews*. 44 (2015) 6187–6229.
 - 420 [3] S. Smith, D. Mager, A. Perebikovskiy, E. Shamloo, D. Kinahan, R. Mishra, S.M. Torres
421 Delgado, H. Kido, S. Saha, J. Ducreé, CD-based microfluidics for primary care in extreme
422 point-of-care settings, *Micromachines*. 7 (2016) 22.
 - 423 [4] M. Tang, G. Wang, S.-K. Kong, H.-P. Ho, A review of biomedical centrifugal microfluidic
424 platforms, *Micromachines*. 7 (2016) 26.
 - 425 [5] C.M. Miyazaki, E. Carthy, D.J. Kinahan, Biosensing on the centrifugal microfluidic lab-on-
426 a-disc platform, *Processes*. 8 (2020) 1360.

- 427 [6] J. Ducrée, Systematic review of centrifugal valving based on digital twin modeling towards
428 highly integrated lab-on-a-disc systems, *Microsystems & Nanoengineering*. 7 (2021) 1–26.
- 429 [7] J. Ducrée, Secure air traffic control at the hub of multiplexing on the centrifugo-pneumatic
430 Lab-on-a-Disc platform, *Micromachines*. 12 (2021) 700.
- 431 [8] J. Ducrée, Design optimization of centrifugal microfluidic “Lab-on-a-Disc” systems to-
432 wards fluidic larger-scale integration, *Applied Sciences*. 11 (2021) 5839.
- 433 [9] J. Ducrée, Anti-counterfeit technologies for microfluidic “Lab-on-a-Disc” systems, *Sensors*
434 and *Actuators A: Physical*. 354 (2023) 114235.
- 435 [10] J. Ducrée, Efficient development of integrated lab-on-a-chip systems featuring operational
436 robustness and manufacturability, *Micromachines*. 10 (2019) 886.
- 437 [11] I. Maguire, R. O’Kennedy, J. Ducrée, F. Regan, A review of centrifugal microfluidics in
438 environmental monitoring, *Analytical Methods*. 10 (2018) 1497–1515.
- 439 [12] S.M.T. Delgado, D.J. Kinahan, L.A.N. Julius, A. Mallette, D.S. Ardila, R. Mishra, C.M.
440 Miyazaki, J.G. Korvink, J. Ducrée, D. Mager, Wirelessly powered and remotely controlled
441 valve-array for highly multiplexed analytical assay automation on a centrifugal microfluidic
442 platform, *Biosensors and Bioelectronics*. 109 (2018) 214–223.
- 443 [13] D.J. Kinahan, S.M. Kearney, N.A. Kilcawley, P.L. Early, M.T. Glynn, J. Ducree, Density-
444 gradient mediated band extraction of leukocytes from whole blood using centrifugo-
445 pneumatic siphon valving on centrifugal microfluidic discs, *PloS One*. 11 (2016) e0155545.
- 446 [14] L.M. Dignan, M.S. Woolf, C.J. Tomley, A.Q. Nauman, J.P. Landers, Multiplexed centrifugal
447 microfluidic system for dynamic solid-phase purification of polynucleic acids direct
448 from buccal swabs, *Analytical Chemistry*. 93 (2021) 7300–7309.
- 449 [15] K. Jackson, J. Borba, M. Meija, D. Mills, D. Haverstick, K. Olson, R. Aranda, G. Garner,
450 E. Carrilho, J. Landers, DNA purification using dynamic solid-phase extraction on a rota-
451 tionally-driven polyethylene-terephthalate microdevice, *Analytica Chimica Acta*. 937
452 (2016) 1–10.
- 453 [16] D.J. Kinahan, R. Burger, D. Lawlor, P.L. Early, A. Vembadi, N.A. McArdle, N.A. Kilcaw-
454 ley, M.T. Glynn, J. Ducrée, Centrifugally automated Solid-Phase Extraction of DNA by
455 immiscible liquid valving and chemically powered centripetal pumping of peripherally
456 stored reagents, *Biosensors and Bioelectronics: X*. 9 (2021) 100085.
- 457 [17] D.J. Kinahan, S.M. Kearney, N. Dimov, M.T. Glynn, J. Ducrée, Event-triggered logical
458 flow control for comprehensive process integration of multi-step assays on centrifugal mi-
459 crofluidic platforms, *Lab on a Chip*. 14 (2014) 2249–2258.
- 460 [18] B.G. Andryukov, Six decades of lateral flow immunoassay: from determining metabolic
461 markers to diagnosing COVID-19, *AIMS Microbiology*. 6 (2020) 280.
- 462 [19] M. Balter, J. Leipheimer, A. Chen, A. Shirao, T. Maguire, M. Yarmush, Automated end-
463 to-end blood testing at the point-of-care: Integration of robotic phlebotomy with down-
464 stream sample processing, *Technology*. 6 (2018) 59–66.
- 465 [20] J. Höfflin, S.M.T. Delgado, F.S. Sandoval, J.G. Korvink, D. Mager, Electrifying the disk: a
466 modular rotating platform for wireless power and data transmission for Lab on a disk appli-
467 cation, *Lab on a Chip*. 15 (2015) 2584–2587.
- 468 [21] K. Sanger, K. Zor, C.B. Jendresen, A. Heiskanen, L. Amato, A.T. Nielsen, A. Boisen, Lab-
469 on-a-disc platform for screening of genetically modified *E. coli* cells via cell-free electro-
470 chemical detection of p-Coumaric acid, *Sensors and Actuators B: Chemical*. 253 (2017)
471 999–1005.

- 472 [22] M. Bauer, J. Bartoli, S.O. Martinez-Chapa, M. Madou, Wireless electrochemical detection
473 on a microfluidic compact disc (CD) and evaluation of redox-amplification during flow,
474 *Micromachines*. 10 (2019) 31.
- 475 [23] S.T. Rajendran, E. Scarano, M.H. Bergkamp, A.M. Capria, C.-H. Cheng, K. Sanger, G. Fer-
476 rari, L.H. Nielsen, E.-T. Hwu, K. Zor, Modular, lightweight, wireless potentiostat-on-a-disc
477 for electrochemical detection in centrifugal microfluidics, *Analytical Chemistry*. 91 (2019)
478 11620–11628.
- 479 [24] S.M.T. Delgado, D.J. Kinahan, F.S. Sandoval, L.A.N. Julius, N.A. Kilcawley, J. Ducreé, D.
480 Mager, Fully automated chemiluminescence detection using an electrified-Lab-on-a-Disc
481 (eLoaD) platform, *Lab on a Chip*. 16 (2016) 4002–4011.
- 482 [25] S.M.T. Delgado, J.G. Korvink, D. Mager, The eLoaD platform endows centrifugal micro-
483 fluidics with on-disc power and communication, *Biosensors and Bioelectronics*. 117 (2018)
484 464–473.
- 485 [26] Z. Noroozi, H. Kido, M.J. Madou, Electrolysis-induced pneumatic pressure for control of
486 liquids in a centrifugal system, *Journal of The Electrochemical Society*. 158 (2011) P130.
- 487 [27] F.O. Romero-Soto, L. Weber, D. Mager, M.M. Aeinehvand, S.O. Martinez-Chapa, Charac-
488 terization of the flow rate on lab-on-a-disc by a low-powered electrolysis pump for wire-
489 less-controlled automation of bioanalytical assays, *Sensors and Actuators B: Chemical*.
490 (2022) 133025.
- 491 [28] M.M. Hoehl, M. Weißert, A. Dannenberg, T. Nesch, N. Paust, F. von Stetten, R. Zengerle,
492 A.H. Slocum, J. Steigert, Centrifugal LabTube platform for fully automated DNA purifica-
493 tion and LAMP amplification based on an integrated, low-cost heating system, *Biomedical*
494 *Microdevices*. 16 (2014) 375–385.
- 495 [29] G. Wang, H.-P. Ho, Q. Chen, A.K.-L. Yang, H.-C. Kwok, S.-Y. Wu, S.-K. Kong, Y.-W.
496 Kwan, X. Zhang, A lab-in-a-droplet bioassay strategy for centrifugal microfluidics with
497 density difference pumping, power to disc and bidirectional flow control, *Lab on a Chip*. 13
498 (2013) 3698–3706.
- 499 [30] M. Tang, J.F.-C. Loo, Y. Wang, X. Zhang, H.-C. Kwok, M. Hui, C.C.-H. Leung, S.-K.
500 Kong, G. Wang, H.-P. Ho, Motor-assisted chip-in-a-tube (MACT): a new 2- and 3-
501 dimensional centrifugal microfluidic platform for biomedical applications, *Lab on a Chip*.
502 17 (2017) 474–483.
- 503 [31] J.M. Chen, P.-C. Huang, M.-G. Lin, Analysis and experiment of capillary valves for micro-
504 fluidics on a rotating disk, *Microfluidics and Nanofluidics*. 4 (2008) 427–437.
- 505 [32] M. Kitsara, C.E. Nwankire, L. Walsh, G. Hughes, M. Somers, D. Kurzbuch, X. Zhang,
506 G.G. Donohoe, R. O’Kennedy, J. Ducreé, Spin coating of hydrophilic polymeric films for
507 enhanced centrifugal flow control by serial siphoning, *Microfluidics and Nanofluidics*. 16
508 (2014) 691–699.
- 509 [33] L. Clime, J. Daoud, D. Brassard, L. Malic, M. Geissler, T. Veres, Active pumping and con-
510 trol of flows in centrifugal microfluidics, *Microfluidics and Nanofluidics*. 23 (2019) 1–22.
- 511 [34] R. Gorkin III, C.E. Nwankire, J. Gaughran, X. Zhang, G.G. Donohoe, M. Rook, R.
512 O’Kennedy, J. Ducreé, Centrifugo-pneumatic valving utilizing dissolvable films, *Lab on a*
513 *Chip*. 12 (2012) 2894–2902.
- 514 [35] C.E. Nwankire, M. Czugala, R. Burger, K.J. Fraser, T. Glennon, B.E. Onwuliri, I.E.
515 Nduaguibe, D. Diamond, J. Ducreé, A portable centrifugal analyser for liver function
516 screening, *Biosensors and Bioelectronics*. 56 (2014) 352–358.

- 517 [36] R. Mishra, J. Zapatero-Rodriguez, S. Sharma, D. Kelly, D. McAuley, S. Gilgunn, R.
518 O’Kennedy, J. Ducree, Automation of multi-analyte prostate cancer biomarker immunoas-
519 say panel from whole blood by minimum-instrumentation rotational flow control, *Sensors*
520 and *Actuators B: Chemical*. 263 (2018) 668–675.
- 521 [37] C.E. Nwankire, A. Venkatanarayanan, T. Glennon, T.E. Keyes, R.J. Forster, J. Ducree, La-
522 bel-free impedance detection of cancer cells from whole blood on an integrated centrifugal
523 microfluidic platform, *Biosensors and Bioelectronics*. 68 (2015) 382–389.
- 524 [38] H. McArdle, E.M. Jimenez-Mateos, R. Raoof, E. Carthy, D. Boyle, H. ElNaggar, N. Delan-
525 ty, H. Hamer, M. Dogan, T. Huchtemann, “TORNADO”–Theranostic One-Step RNA De-
526 tector; microfluidic disc for the direct detection of microRNA-134 in plasma and cerebro-
527 spinal fluid, *Scientific Reports*. 7 (2017) 1–11.
- 528 [39] B.D. Henderson, D.J. Kinahan, J. Rio, R. Mishra, D. King, S.M. Torres-Delgado, D. Mager,
529 J.G. Korvink, J. Ducree, Siphon-controlled automation on a lab-on-a-disc using event-
530 triggered dissolvable film valves, *Biosensors*. 11 (2021) 73.
- 531 [40] D.J. Kinahan, M. Renou, D. Kurzbuch, N.A. Kilcawley, É. Bailey, M.T. Glynn, C.
532 McDonagh, J. Ducree, Baking powder actuated centrifugo-pneumatic valving for automa-
533 tion of multi-step bioassays, *Micromachines*. 7 (2016) 175.
- 534 [41] C.M. Miyazaki, D.J. Kinahan, R. Mishra, F. Mangwanya, N. Kilcawley, M. Ferreira, J. Du-
535 cree, Label-free, spatially multiplexed SPR detection of immunoassays on a highly inte-
536 grated centrifugal Lab-on-a-Disc platform, *Biosensors and Bioelectronics*. 119 (2018) 86–
537 93.
- 538 [42] R. Uddin, D. Kinahan, J. Ducree, A. Boisen, Lab-on-a-disk extraction of PBMC and me-
539 tered plasma from whole blood: An advanced event-triggered valving strategy, *Biomicro-*
540 *fluidics*. 15 (2021) 064102.
- 541 [43] D.J. Kinahan, S.M. Kearney, O.P. Faneuil, M.T. Glynn, N. Dimov, J. Ducree, Paper imbib-
542 ition for timing of multi-step liquid handling protocols on event-triggered centrifugal micro-
543 fluidic lab-on-a-disc platforms, *RSC Advances*. 5 (2015) 1818–1826.
- 544 [44] D.J. Kinahan, F. Mangwanya, R. Garvey, D.W. Chung, A. Lipinski, L.A. Julius, D. King,
545 M. Mohammadi, R. Mishra, M. Al-Ofi, Automation of silica bead-based nucleic acid ex-
546 traction on a centrifugal lab-on-a-disc platform, in: *IOP Publishing*, 2016: p. 012013.
- 547 [45] R. Mishra, R. Alam, D. McAuley, T. Bharaj, D. Chung, D.J. Kinahan, C. Nwankire, K.S.
548 Anderson, J. Ducree, Solvent selective membrane routing and microfluidic architecture to-
549 wards centrifugal automation of customisable bead based immunoassays, *Sensors and Ac-*
550 *tuator B: Chemical*. 356 (2022) 131305.
- 551 [46] R. Mishra, L.A. Julius, J. Condon, P. Pavelskopfa, P.L. Early, M. Dorrian, K. Mrvova, G.
552 Henihan, F. Mangwanya, T. Dreo, Plant pathogen detection on a lab-on-a-disc using solid-
553 phase extraction and isothermal nucleic acid amplification enabled by digital pulse-actuated
554 dissolvable film valves, *Analytica Chimica Acta*. 1258 (2023) 341070.
- 555 [47] B.R. Lutz, P. Trinh, C. Ball, E. Fu, P. Yager, Two-dimensional paper networks: program-
556 mable fluidic disconnects for multi-step processes in shaped paper, *Lab on a Chip*. 11
557 (2011) 4274–4278.
- 558 [48] Z. Zhakypov, M. Mete, J. Fiorentino, J. Paik, Programmable fluidic networks design for
559 robotic origami sequential self-folding, in: *IEEE*, 2019: pp. 814–820.
- 560 [49] S. Tsuda, H. Jaffery, D. Doran, M. Hezwani, P.J. Robbins, M. Yoshida, L. Cronin, Custom-
561 izable 3D printed ‘plug and play’ millifluidic devices for programmable fluidics, *PLoS One*.
562 10 (2015) e0141640.

- 563 [50] P. Zucchelli, B. Van de Vyver, Dosimeter for programmable microscale manipulation of
564 fluids, US8226908B2, 2012.
- 565 [51] L. Morelli, L. Seriola, F.A. Centorbi, C.B. Jendresen, M. Matteucci, O. Ilchenko, D. De-
566 marchi, A.T. Nielsen, K. Zór, A. Boisen, Injection molded lab-on-a-disc platform for
567 screening of genetically modified E. coli using liquid–liquid extraction and surface en-
568 hanced Raman scattering, Lab on a Chip. 18 (2018) 869–877.
569